



SNAMES ~ MAN DIESEL Industry Nite



Brief Profile of Speakers:



Mr. Lars Bryndum
Director of Customer Support

Lars Bryndum, born 1949, received his M.Sc. in Mechanical Engineering from the Technical University of Denmark, Lyngby, in 1974.

After his graduation, Lars Bryndum worked five years at the Danish Maritime Institute, Copenhagen, where he was involved in ship propulsion and propeller design.

Lars Bryndum joined A/S Burmeister & Wain's Motor- og Maskinfabrik after 1971 A/S in 1979 and worked ten years with vibration aspects in the Research and Development department.

In 1990, he was transferred as a section manager to Two-stroke Design and in 1995, he was appointed to Senior Manager of Large Bore Engine Design.

In 2000, Lars Bryndum was appointed to Representative Director of MAN B&W Diesel in Korea and was the Managing Director of the office in Busan, Korea.

From 1 September 2006, Lars Bryndum has been Director in the department for Customer Support at the head office for two-stroke engines in Copenhagen, Denmark.



Mr. Stig Baungaard Jakobsen
Senior Manager of Two-Stroke Operations

Stig Baungaard Jakobsen holds a M.Sc. in Mechanical Engineering, obtained from the Technical University of Denmark in 1982.

Jakobsen joined MAN B&W Diesel's Two-stroke R&D Department in Copenhagen in 1982. He worked there as a vibration specialist until 1990 when he was appointed Manager of the Vibration Analysis Section.

In 1999, he subsequently became Manager of the Engine Development Section, followed by becoming Senior Manager of the New Design Department in 2001.

Three years later, Stig Baungaard Jakobsen was appointed Vice President of High Speed Diesel Engineering at MAN Diesel, Stockport, England and has been Senior Manager of MAN Diesel's Two-stroke Operation Department in Copenhagen since 2005.

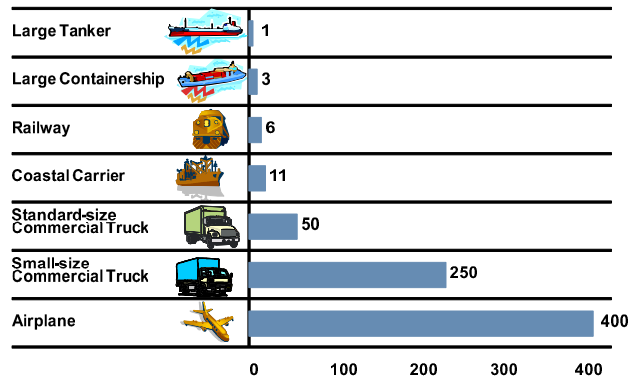
Challenging Times

Lars Bryndum
Director Customer Support
Marine Low Speed Engineering

- Fuel cells Need development and clean fuel
 Need frequency converters and el. motors.
- Sun and wind Need development and back-up
- Nuclear power Politically and economically not feasible

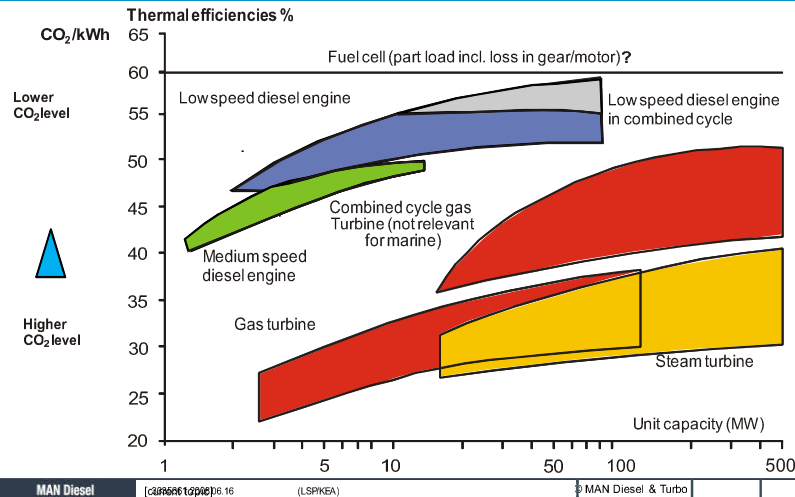
**For a foreseeable future
Diesels will prevail
..... using cleaner and less fuels**

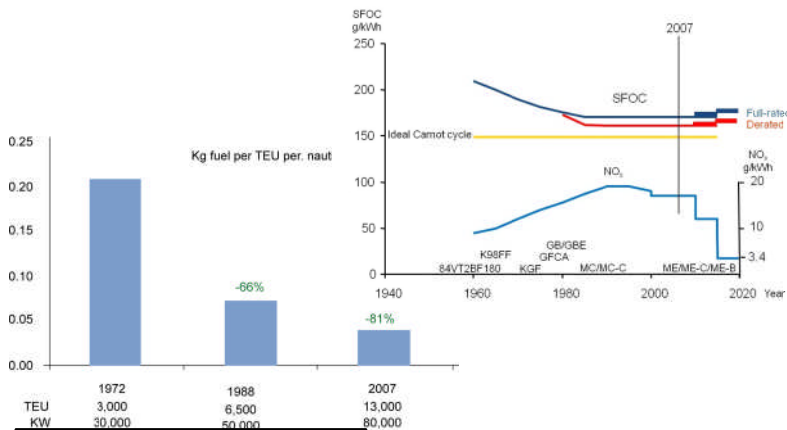
CO₂ Emissions per Unit Load by Transport Mode



Source: Report on Research for CO₂ Emission from Ships 2000 (SOF, Japan)
Interim Report by Transport Policy Council 2006 (MLIT, Japan)
Common Guideline for Calculation Method of CO₂ Emission in Logistics (Issued on 2006 by METI and MLIT)

Typical Thermal Efficiency of Prime Movers





Made possible with larger engines

Alternative fuels for two-stroke diesel engines.

- LNG
- Bio fuels
- Any hydrocarbon
- Hydrogen
- Orimulsion
- Coal slurry
- Synthetic fuels ??

Two-stroke Engine Programme
2010 3rd edition



Dot 2 engines



MAN B&W Low Speed Propulsion Engines

The tables below summarise the possibilities available with the MAN B&W type engines. All SFOC figures are relative to the SFOC at 100% load for a standard engine.

- ECT: Engine Control Tuning
- VT: Variable Turbine Area
- EGS: Exhaust Gas Bypass

IMO regulated low speed	loading methods	0%	25%	50%	75%	100%
MICE 1000	Standard L engine	0.0	+1	-0.5	-0.5	0
MICE 1000	ECT	2.5	-2	-4.5	-4.5	0
MICE 1000	VT	2.5	-4	-6.5	-6.5	0.5
MICE 1000	EGS	0.5	-4	-6.5	-6.5	1.5
MICE 1000	ECT	1	-3.5	-6	-6.5	1.5
MICE 1000	VT	-1.5	-6	-6.5	-6.5	2.5
MICE 1000	EGS	-1.5	-6	-6.5	-6.5	1.5

Table 2: Optimisation possibilities - MICE/C-series engines, SMOX+L

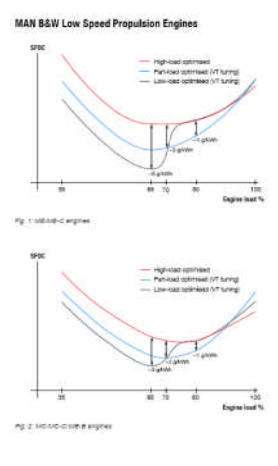
IMO regulated low speed	loading methods	0%	25%	50%	75%	100%
MICE 1000	Standard L engine	0	0	-0.5	-0.5	0
MICE 1000	VT	2	-2	-3.5	-4	0
MICE 1000	EGS	2	-2	-3.5	-4	0
MICE 1000	VT	1	-2	-3.5	-4	1
MICE 1000	EGS	1	-3	-3.5	-4	2

For a specific L engine, the SFOC profile can be found directly from the above tables. For example, an SMOX-C8.2 running at 85% load with an SFOC of 169 g/kWh and optimised for peak load with VT tuning has a consumption of 169 + 6.5 g/kWh = 175.5 g/kWh.

The above tuning methods are also available for detuned engines with different SMOX. The standard SFOC profile at load is different for a detuned engine, but the above difference between each tuning method and the standard engine will be the same.

Only high-load optimisation is possible for engines with conventional efficiency turbochargers.

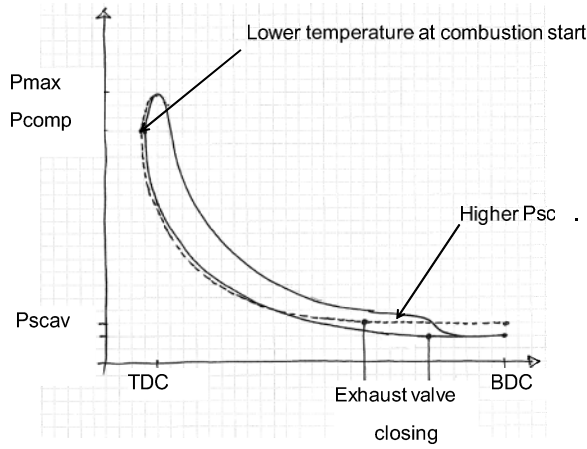
The methods and options mentioned will be explained in the following.



Tier II Evolution continued

- Increased scavange air pressure later closing of exhaust valve (enhanced Miller timing). Available with proven MAN Diesel & Turbo TCA turbochargers. New generation of ABB and MET turbocharger required.
- Reduced compression ratio
- Increased maximum combustion pressure
- Adjustments of compression volume
- Design changes on Pmax influenced components (mainly cylinder liner, piston, cover and crossheads)
- General outlines, dimensions, stroke, etc., have been kept unchanged.

S80ME-C8/9 = original Mk 8/9 engine complying with Tier I
S80ME-C8.1/9.1 = original Mk 8/9 engine complying with Tier II
S80ME-C8.2/9.2 = the new fuel-optimised version complying with Tier II



1. SFOC optimised load ranges

- High Load: 85% - 100% SMCR (standard tuned engine)
- Part Load: 50% - 85% SMCR
- Low Load: 25% - 70% SMCR

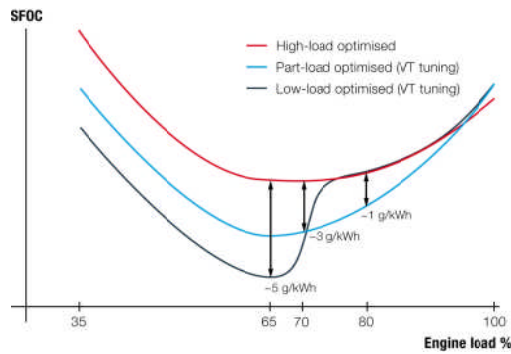
2. Engine tuning methods available for part load and low load optimisations

- EGB: Exhaust Gas Bypass
- VT: Variable Turbine Area
- ECT: Engine Control Tuning (only for ME/ME-C)
- Only available for engines with high-effective turbocharger*

3. Examples are shown for the below two engine types

6S80ME-C8.2 and 6S80MC-C8.2

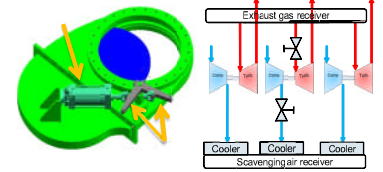
ME / ME-C engines – example with VT:



Exhaust Gas By-pass, EGB



Turbocharger Cut-out

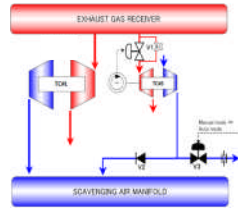


Turbocharger Variable Turbine Area, VTA

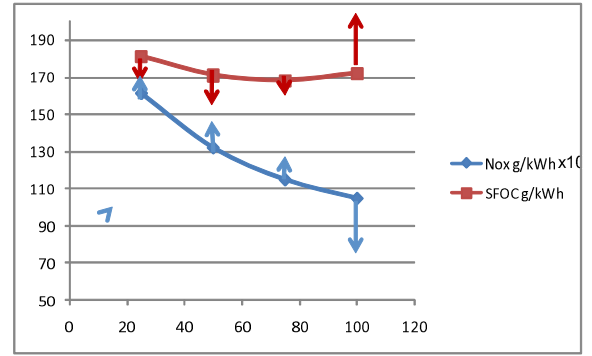
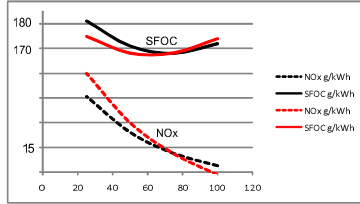




Sequential Turbocharging



ECT Engine Control Tuning
SFOC-NO_x Balancing

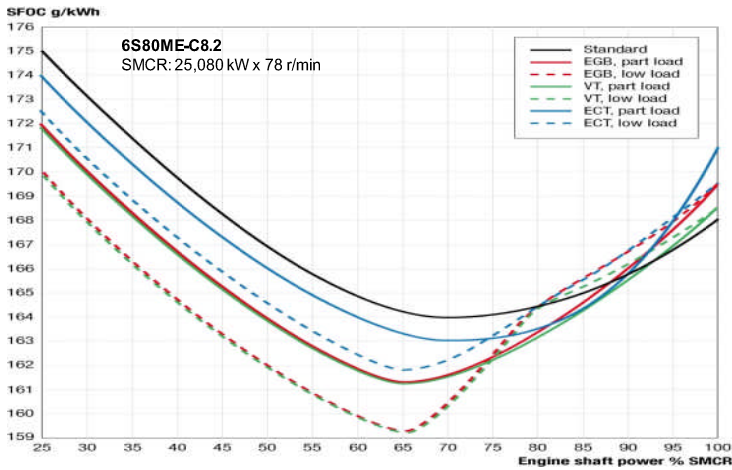


E3 Cycle = 5%*NOx(25) + 11%*NOx(50) + 55%*NOx(75) + 29%*NOx(100) < 14,4 g/kWh

SFOC Optimisation Methods – IMO Tier II Engines



SFOC Optimisation Methods – IMO Tier II Engines



Load Profile →

Main engine 6S80ME-C8.2 IMO Tier II
SMCR = 25,080kW x 78r/min

Standard engine, high load optimised

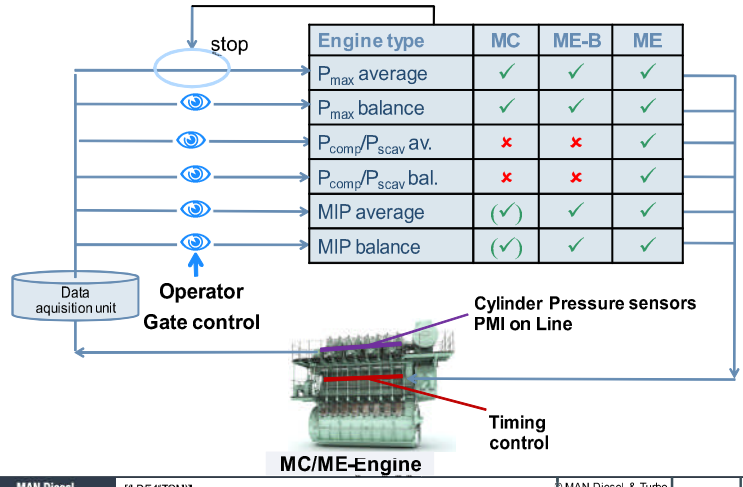
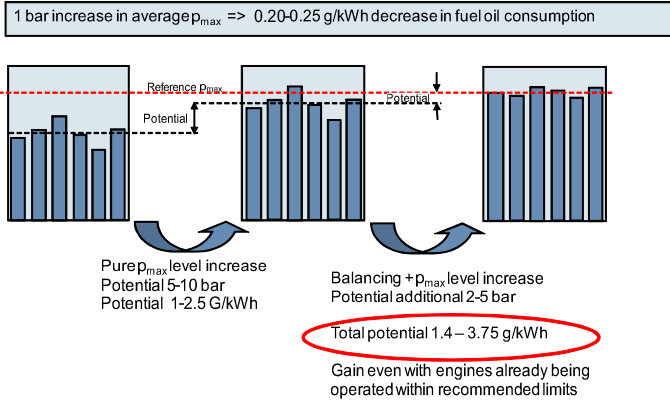
Engine load	% SMCR	35%	50%	65%	85%	100%	Total fuel consumptions
Engine power	kW	8,778	12,540	16,302	21,318	25,080	
SFOC	g/kWh	171.4	167.0	164.3	165.0	168	
Re LCV = 42,700 kJ/kg							
Fuel consumption	t/day	36.1	50.3	64.3	84.4	101.1	
Days in service	day/year	40	100	90	15	5	
Fuel consumption	t/year	1,444	5,030	5,787	1,266	505	14,033 t/year

VT, low load optimised

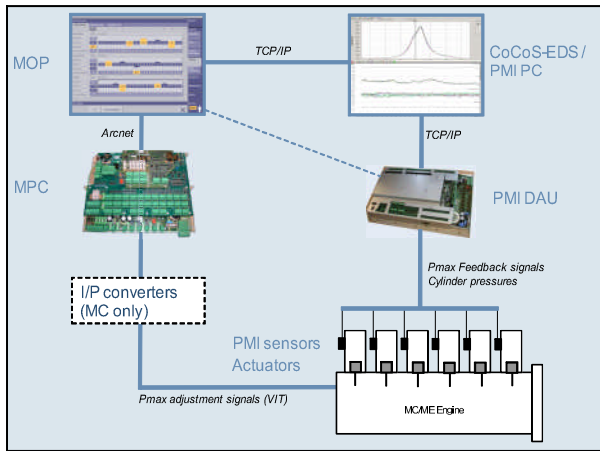
Engine load	% SMCR	35%	50%	65%	85%	100%	Total fuel consumptions
Engine power	kW	8,778	12,540	16,302	21,318	25,080	
SFOC	g/kWh	166.4	162.0	159.3	165.3	168.5	
Re LCV = 42,700 kJ/kg							
Fuel consumption	t/day	35.0	48.8	62.3	84.6	101.4	
Days in service	day/year	40	100	90	15	5	
Fuel consumption	t/year	1,400	4,880	5,607	1,269	507	13,663 t/year
Fuel savings	t/year	44	150	180	-3	-1	370 t/year
Fuel savings	%/year	3.0	3.0	3.0	-0.2	-0.3	2.6%/year



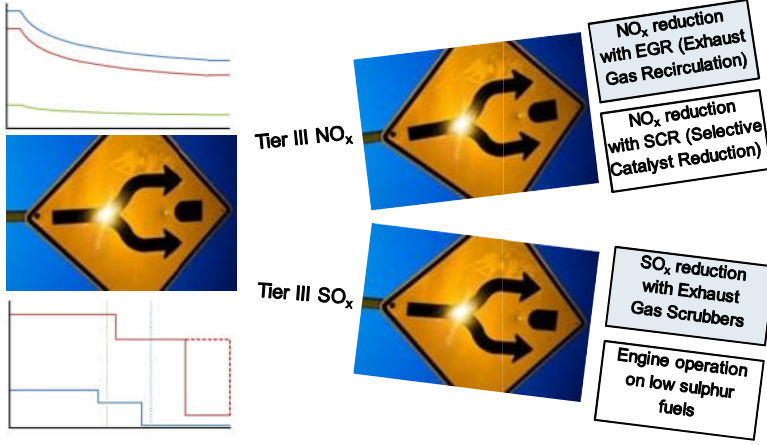
Reduction in fuel oil consumption / CO₂ emission

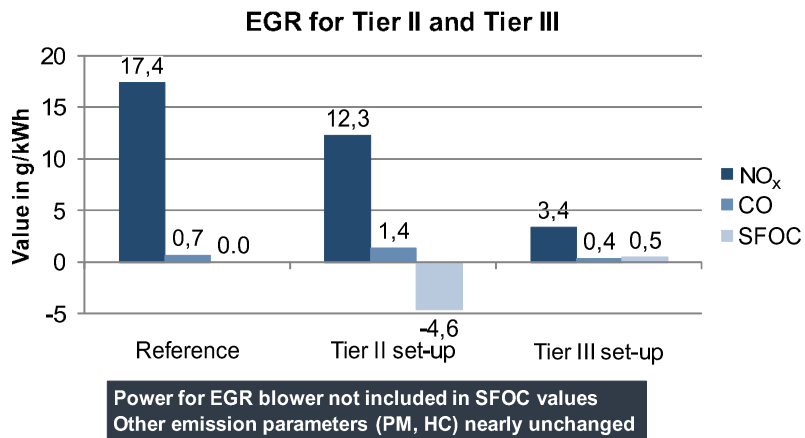
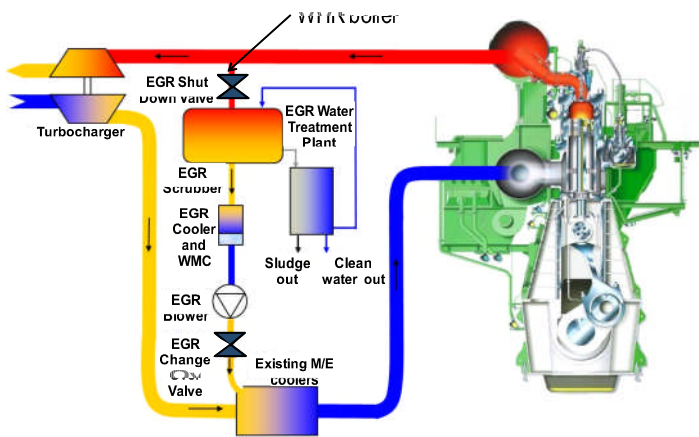


Auto tuning: ME & MC engines



Flexible and Agile Two-Way Approach for Fulfilling IMO Tier III

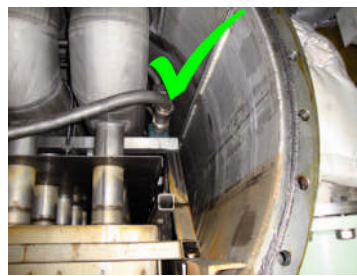
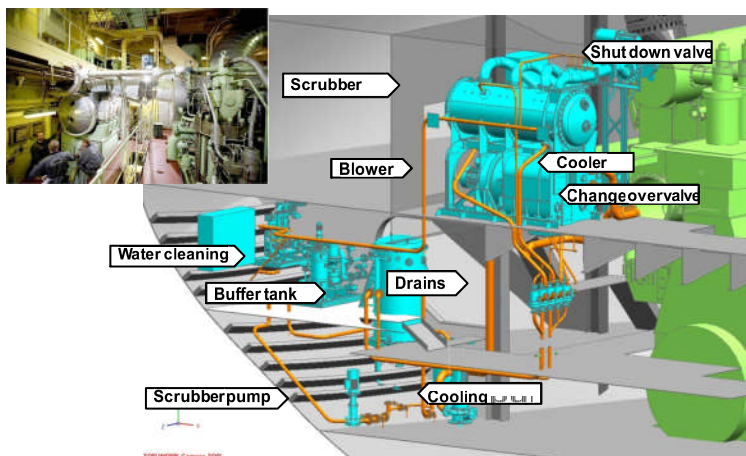




Arrangement in Engine Room



System Inspection



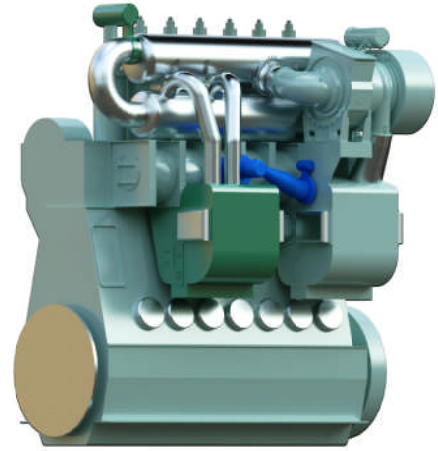
Scrubber condition is fine



EGR cooler and WMC is fine



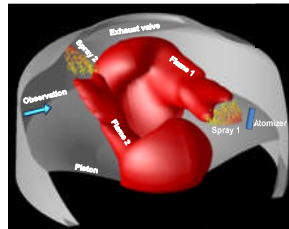
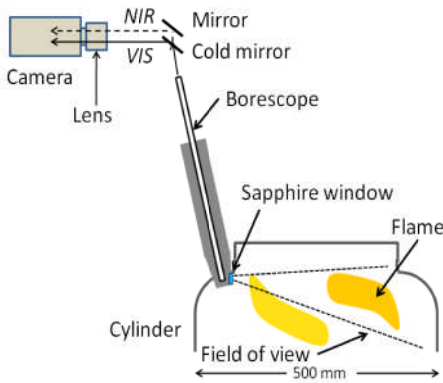
- EGR control system performed as planned
- Scrubber, blower and EGR cooler had sufficient capacity
- Pumps, drainers and buffer tank performed well
- Scrubber unit in perfect condition
- M/E coolers and WMC's looked fine – no deposits or corrosion
- NO_x reduction better than expected
- ? Water Cleaning unit and PH dosing system not operating as expected
- ? Cylinder condition not confirmed, only due to too short operation time



Photographing Combustion



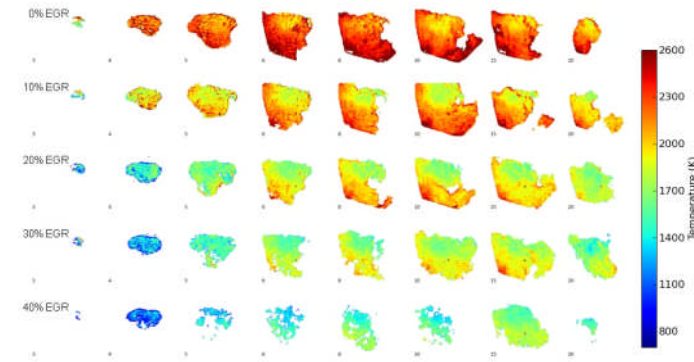
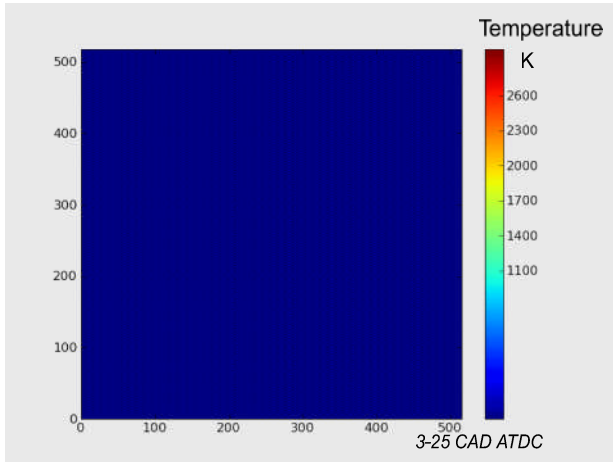
High Speed Imaging of Combustion



Recording with

- 18,000 frames per seconds
- Shuttertime 4μs

Combustion slowed down 600 times!



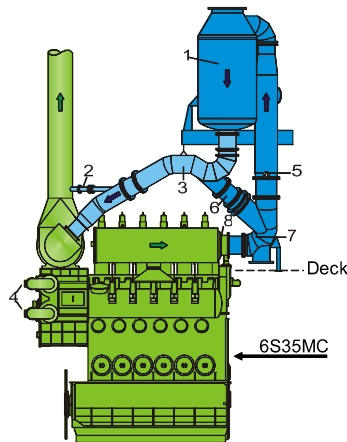
SCR Selective Catalytic Reactor



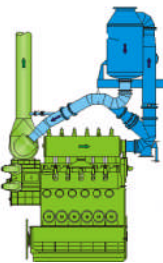
Objectives and Cooperation Partner



- 1 SCR reactor
- 2 Turbocharger bypass
- 3 Temperature sensor after SCR
- 4 Large motors for auxiliary blowers
- 5 Urea injector
- 6 SCR bypass
- 7 Temperature sensor before SCR
- 8 Additional flange in exhaust gas receiver



- Objectives
 - Develop commercial high-pressure SCR solutions
 - Meet Tier III requirements as only installed NO_x reducing technology
 - Applicable with MC, ME and ME-B engines
 - High "fuel tolerance"
- Three partners
 - MAN Diesel & Turbo Copenhagen
 - Engine builder
 - Catalyst manufacturer



- Upgrade from **Tier 0 to Tier I (NO_x)**
- Engines installed on year **1990 to 2000** ships
 - Cyl displ. ≥90L & Engine power >5000kW
 - Approved Method available
- Regulation into force **1. July 2010**



The Approved Method is available when:

- The **designer** of the base engine to which the Approved Method applies, verifies that:
 - **engine rating** is not reduced by more than 1.0%
 - **Specific Fuel Oil Consumption** is not increased by more than 2.0%
 - **engine durability** and **reliability** is not adversely affected
- The **cost** of the Approved Method is not excessive

Approved Method

An Approved Method for an MAN B&W engine consists of a slide valve (with a newly developed low-NO_x nozzle) and, in some cases, minor performance adjustments.

The application of an MAN B&W Approved Method will result in a range of benefits, among others:

- compliance with MARPOL Annex VI, Regulation 13, chapter 7
- unchanged or slightly improved fuel oil consumption
- reduced emissions of NO_x, carbon monoxide, hydrocarbons and particulate matter
- improved low-load operation
- cleaner combustion chamber and exhaust gas ways.

The first engine type to receive an Approved Method is the S70MC. The S60MC and S50MC will follow during the second half of 2010.

Approved Method

It is the ship owner's obligation (when a vessel renewal survey is coming up following 1 July 2010) to verify whether an Approved Method has been released for his specific engine.

If an Approved Method is available, the ship owner shall introduce the Approved Method on board at the renewal survey.

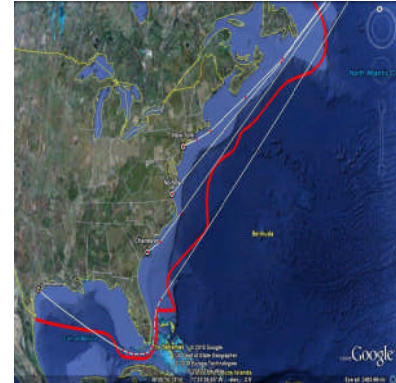
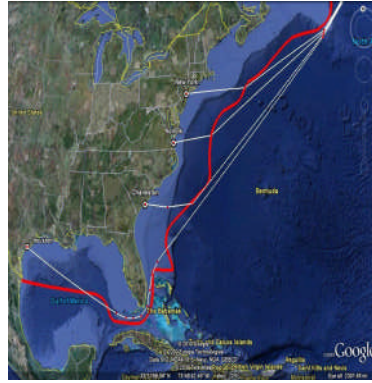
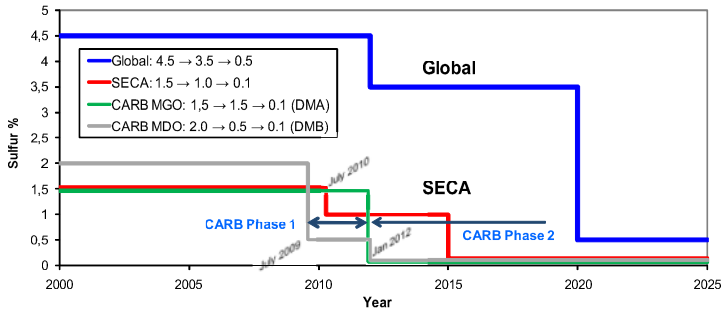
If no Approved Method is available, the engine is in compliance, but the Class must amend the new IAPP that no Approved Method exists.

<http://www.mandieselturbo.com/AM>

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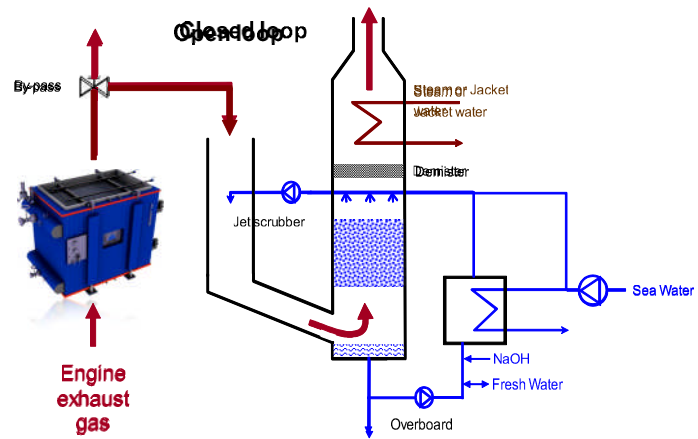
MEPC 58 IMO & CARB Fuel-Sulfur Content Limits
Equivalent methods may be used as alternative

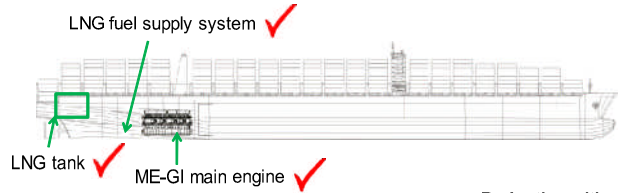
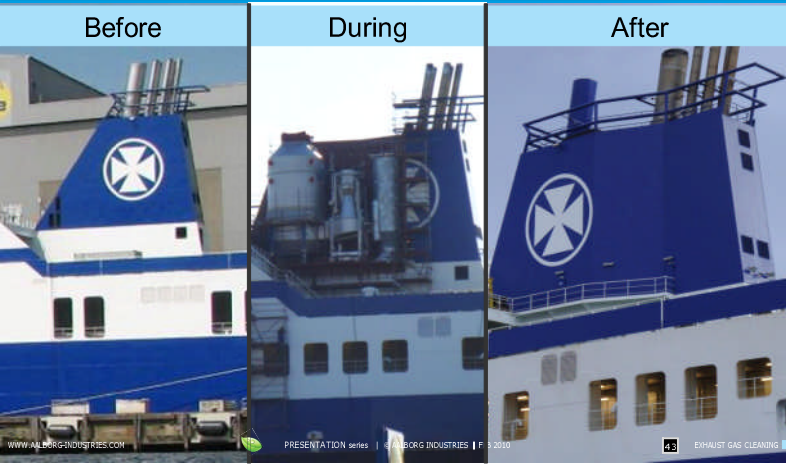


SOx Removal with Wet Scrubber



Scrubber Operation



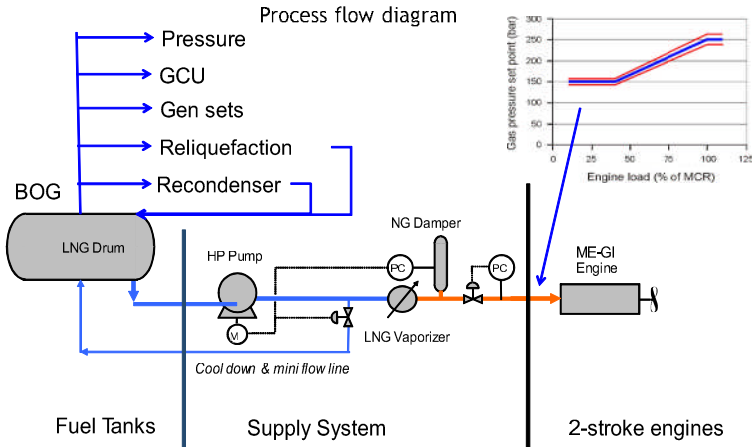


	Reduction with ME-GI	Reduction with ME-GI + WHR	Reduction with ME-GI + WHR+EGR
CO ₂ (gram per tonne mile)	23%	35%	33%
NO _x (gram per tonne mile)	13%	13%	80%
SO _x (gram per tonne mile)	92%	92%	94%
Particulate matter (mg per m ³)	37%	37%	48%

LNG as Fuel for Marine Propulsion



ME-GI: Gas and Pilot Oil Injection



Background

- Dual fuel experience since 1994
- Well-proven ME technology

New components

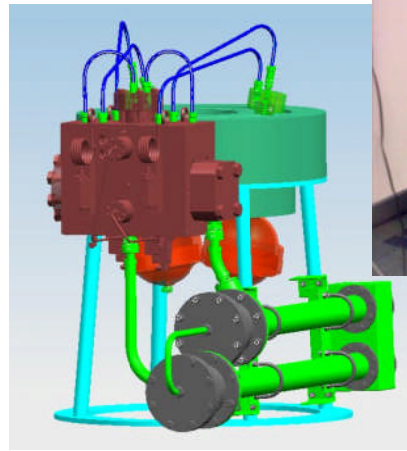
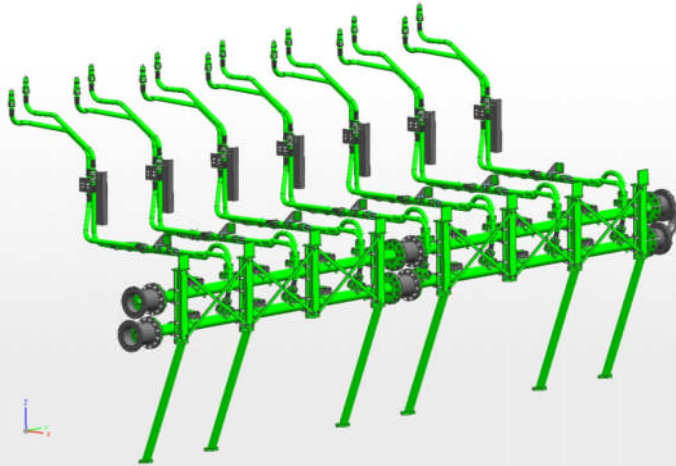
- Double wall gas pipes
- Gas Injections valves
- Large volume accumulators
- ELGI valves
- Control and safety system

Modified components

- Cylinder cover
- Exhaust receiver

4T50ME-GI ready for type approval test January 2011

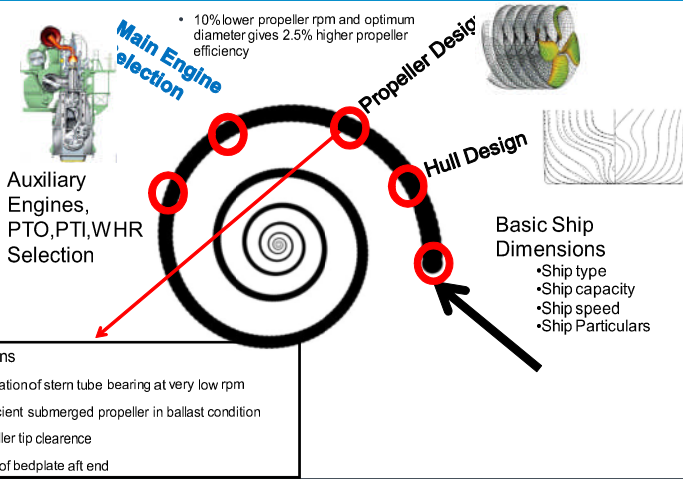




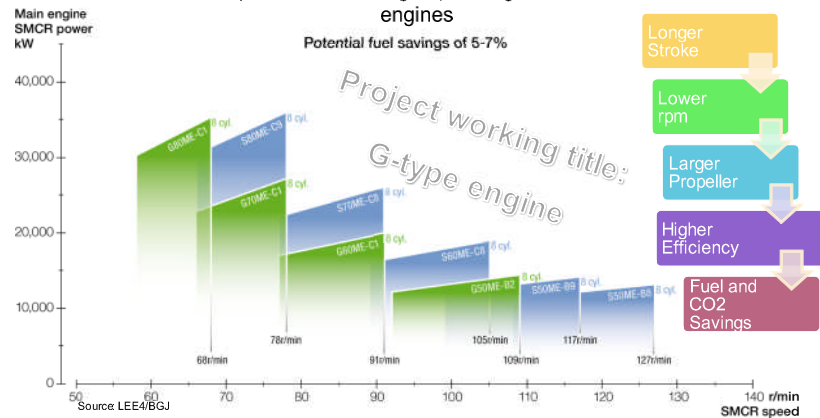
Design Spiral

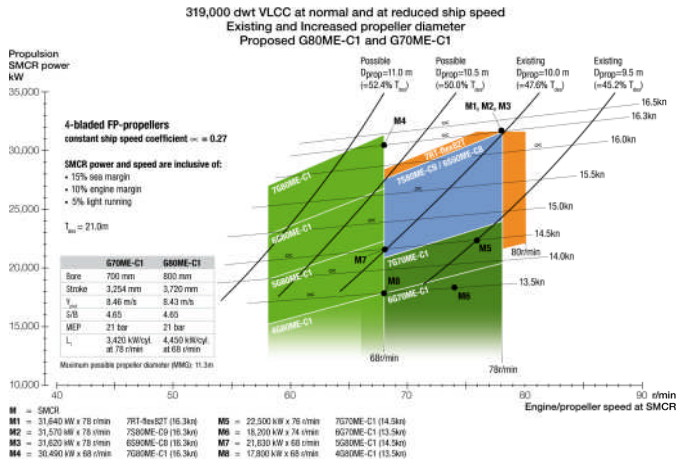


G-ME Engines



Layout diagrams of proposed series of G-ME engines compared with existing super long stroke S-ME engines





- Tier II or Tier III, 2015
- Operation pattern in known and future ECAs
- Economical service speed
- Fuel types and prices
- NO_x, SO_x and PM abating equipment
- Preparation beyond existing rules
- Resale price of vessel
- CO₂ energy efficiency considerations
- Low load layout
- Waste Heat Recovery
- And much more outside the engine room

